

Semiconductor thermogenerator - Seebeck effect

(Item No.: P2410700)

Curricular Relevance



Keywords:

Seebeck effect (thermoelectric effect), thermoelectric e.m.f., efficiency, Peltier coefficient, Thomson coefficient, Seebeck coefficient, direct energy conversion, Thomson equations

Overview

Short description

In a semi-conductor thermogenerator, the no-load voltage and the short-circuit current are measured as a function of the temperature difference. The internal resistance, the Seebeck coefficient and the efficiency are determined.







Equipment

| Position No. | Material | Order No. | Quantity |
|--------------|--|-----------|----------|
| 1 | Thermogenerator with 2 water baths | 04366-00 | 1 |
| 2 | Flow-through heat exchanger | 04366-01 | 2 |
| 3 | Heat conductive paste,50 g | 03747-00 | 1 |
| 4 | Connection box | 06030-23 | 1 |
| 5 | Rheostat, 33 Ohm , 3.1A | 06112-02 | 1 |
| 6 | Voltmeter,0.3-300VDC,10-300VAC / | 07035-00 | 1 |
| 7 | Ammeter 1/5 A DC | 07038-00 | 1 |
| 8 | Stopwatch, digital, 1/100 s | 03071-01 | 1 |
| 9 | Immersion thermostat Alpha A, 230 V | 08493-93 | 1 |
| 10 | External circulation set f. thermostat Alpha A | 08493-02 | 1 |
| 11 | Bath for thermostat, makrolon | 08487-02 | 1 |
| 12 | Lab thermometer,-10+100 °C | 38056-00 | 1 |
| 13 | Thermometer -10+50 °C | 38034-00 | 1 |
| 14 | Resistor 10 Ohm 2%, 2W, G1 | 06056-10 | 1 |
| 15 | Resistor 2 Ohm 2%, 2W, G1 | 06055-20 | 1 |
| 16 | Resistor 1 Ohm 2%, 2W, G1 | 06055-10 | 1 |
| 17 | Resistor 5 Ohm 5%, 2W, G1 | 06055-50 | 1 |
| 18 | Rubber tubing, i.d. 6 mm | 39282-00 | 4 |
| 19 | Tubing connector, ID 6-10mm | 47516-01 | 2 |
| 20 | Connecting cord, 32 A, 500 mm, red | 07361-01 | 3 |
| 21 | Connecting cord, 32 A, 500 mm, blue | 07361-04 | 2 |



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Tasks

- 1. To measure no-load voltage $U_{\rm o}$ and short-circuit current $I_{\rm s}$ at different temperature differences and to determine the Seebeck coefficient.
- 2. To measure current and voltage at a constant temperature difference but with different load resistors, and to determine the internal resistance $R_{\rm i}$ from the measured values.
- 3. To determine the efficiency of energy conversion, from the quantity of heat consumed and the electrical energy produced per unit time.

Set-up and procedure

The experiment is set up as shown in Fig. 1.

1. Secure flow-type heat exchangers to each side of the thermogenerator. Fill the cold side with tap water and set the temperature of the hot side on the thermostat. The two temperatures are measured using the holes in the thermogenerator provided for the purpose. The short-circuit current and the noload voltage are measured directly, the internal resistance of the measuring equipment being disregarded.



2. Connect rheostat $R_{\rm ext.}$ to the thermogenerator at a constant average temperature difference. Measure the current and voltage at different settings and plot the results on a graph.

3. Remove the heat exchanger which was connected to the thermostat and put a water bath brim-full of boiling water in its place. Measure the temperature of the hot side $T_{\rm h} = f(t)$ and of the cold side $T_{\rm c} = f(t)$ as a function of time. Measure the current and the voltage across an external resistance of approximately the same value as the internal resistance.

Theory and evaluation

If a temperature drop is created along a current-free branch of a conductor made up of different materials, heat flows from the warmer region to the cooler one. The charge carriers which take part in this transfer of heat are unevenly distributed along the conductor. An internal field strength is set up, which can be shown to be the e.m.f. $U_{\rm o}$ at the open ends of the conductor (Seebeck effect).

The voltage level depends on the temperature difference and on the materials used. To a first approximation, the voltage may be written:

$$U_{
m o}=lpha_{
m 1,2}(T_{
m h}-T_{
m c})=lpha_{
m 1,2}\Delta T$$

where $\alpha_{1,2}$ is the Seebeck coefficient of the combination of materials used, $T_{\rm h}$ is the temperature of the hot side and $T_{\rm c}$ the temperature of the cold side.

1. Applying the regression expression

 $U_{
m o} = a + b\Delta T$

to the measured values in Fig. 3, we obtain

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 $b=0.0587rac{\mathrm{V}}{\mathrm{K}}$ with the standard error $s_\mathrm{b}=0.0006rac{\mathrm{V}}{\mathrm{K}}$



The thermogenerator consists of 142 elements connected in series. The Seebeck coefficient of the semiconductor combination used is therefore

 $\alpha_{1,2} = 4.13 \cdot 10^{-4} \frac{V}{K}$

with the standard error

 $s_{lpha 1,2} = 4.04 \cdot 10^{-4} rac{\mathrm{V}}{\mathrm{K}}$

As the short-circuit also increases linearly with the temperature, the internal resistance of the thermogenerator is constant in the temperature range considered.



2. Applying the regression expression $U\!=\!a+bI$ to the measured values from Fig. 5 we obtain



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$$\begin{split} & a = U_{\rm o} = 2.34 \ {\rm V} \\ & s_{\rm a} = s_{{\rm U}_{\rm o}} = 0.01 \ {\rm V} \\ & \text{and} \\ & |b| = R_i = 2.80 \ \Omega \\ & s_{\rm b} = s_{{\rm R}_i} = 0.02 \ \Omega \\ & \text{and the short circuit current} \\ & I_{\rm s} = \frac{U_{\rm o}}{R_{\rm i}} = 0.84 \ {\rm A} \\ & \text{with} \\ & s_{{\rm I}_{\rm s}} = 0.01 \ {\rm A} \end{split}$$



3. From Fig. 6 we determine the slope of the (descending) curve at one point by drawing a tangent or by linear regression.



At a temperature difference ΔT of 40 K we obtain the following for the nearest measured values, using the regression expression $\Delta T = a + bt$:

$$b = rac{d\Delta T}{dt} = -0.0361 rac{\mathrm{K}}{\mathrm{s}}$$

We can thus work out the quantity of heat Q flowing through the generator in unit time in accordance with

$$\frac{dQ}{dt} = P_{\text{th.}} = C \cdot \left(\frac{d\Delta T}{dt}\right)$$

As the mass of water $m_w\,{=}\,0.194~{
m kg}$ and the specific heat capacity if water

 $c_{\mathrm{w}} = 4182 \frac{\mathrm{J}}{\mathrm{K}}$

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we obtain

$$C = m_{\mathrm{w}} \cdot c_{\mathrm{w}} = 811 rac{\mathrm{J}}{\mathrm{kg K}}$$

so that

$$P_{\mathrm{th.}} = 29.3 \frac{\mathrm{J}}{\mathrm{s}}$$

The electrical power, measured at constant load, $P_{\rm el.}$, can be obtained from Fig. 7. For a temperature difference $\Delta T = 40~{\rm K}$ we obtain $P_{\rm el.} = 0.25~{\rm W}$, so that the efficiency

 $\eta \,{=}\, rac{P_{
m el.}}{P_{
m th.}} \,{=}\, 0.009 \ {
m or} \ 0.9\%$





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